



Cutting temperature measurement in turning of thermoplastic composites using a tool-work thermocouple

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Abstract

Turning of carbon fibre reinforced thermoplastic pipes is used for production of fluid ducts for the aerospace and oil industries. Although thermoplastics are chemically stable, the matrix could be affected by the heat introduced by the machining process. This paper presents how to measure cutting temperature using C/PEEK and C/PA12 material as examples. A suitable method based on a thermocouple circuit and electric conductivity of the carbon fibres is presented, including system calibration. Measurement uncertainties were established for this new method of calibration and measurement for both tested materials. The cutting temperature measurements were analysed by ANOVA and significant factors and its dependence on temperature were identified for further machining process optimization and determination of the predictive model equation. This mathematical cutting temperature model was estimated based on the measurements, and empirical coefficients were identified for selected statistically significant parameters for both composite materials. Because the measured temperatures were above the melting point, the machined surface, chips and structural changes of polymeric matrices were measured in order to prove heat affection.

Keywords Thermoplastic composites · Turning · Cutting temperature measurement

1 Introduction

Increasing the useful properties of the structural element is essential for improving product design. One way to achieve this is to reduce the part's weight when its mechanical properties are fixed or improved by a combination of two or more different types of construction materials. Materials with two or more components are called composites and combine the properties of a reinforcement and the properties of the matrix. Polymer composites with fibre reinforcement are suitable for construction parts under low stress or structural elements of machines mainly for decreasing the entire weight of a product

[1]. The fibres of reinforcements are typically glass, carbon or natural. Polymer matrices are thermosets or thermoplastics. The choice of matrix and fibre type, the matrix-fibre volume ratio and the orientation of the reinforcement in the composite influence the resulting mechanical properties as well as work-piece machinability. The most commonly used combinations are glass or carbon fibres in the thermoset matrix [2].

Thermoplastic matrices are used less often than composites with a resin matrix. Thermoplastic matrices have some technological advantages, including, for example, the possibility of post-process hot forming and better recyclability [3]. Thermoplastic composites have better machinability in comparison to thermosets because fewer dust particles are produced during machining and there is a lower tendency to delamination [4]. Thermoplastics with carbon fibres are used in the aircraft and automotive industries but they have also penetrated other sectors of industry. The entire processing chain of composite parts was described by Fleischer [5]. One of the main problems of composite parts is quality after machining. Thermoplastic composites are machined to achieve dimensional and shape accuracy or to prepare functional surfaces. Quality problems, such as delamination, thermal influence of the machined surface or surface roughness, are discussed through all types of machining technologies, e.g. [6–9]. The

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quality can be monitored in the process indirectly by measuring the cutting force, the cutting temperature and the wear of the cutting tool, if the relationship between these quantities and the evaluated surface quality is known. Mechanical loads can be reduced by reducing cutting force through cutting conditions, especially feed, and then also by optimizing the tool geometry. The heat generation is also affected by the geometry of the cutting tool, but mainly also by the cutting speed. Due to the low thermal conductivity of polymer matrices, the heat concentration at the cutting edge can be a serious problem for the quality of the machined surface.

Thermoplastic composites are machined in order to obtain dimensional and shape accuracy or to prepare functional surfaces. Drilling operations are used for preparing of holes for joining. It is the most commonly used cutting technology for machining composite parts and has been researched in many studies. They focus mainly on the quality of enter and exit of the hole, e.g. [10–12], but a smaller amount is also focused on measuring the temperature during drilling, e.g. [13–15]. The second widely used cutting technology is milling. Composite part milling is used to trim composite surpluses at the edges of the part after forming. Milling technology studies are very often focused on delamination and how to prevent it, e.g. [16–18]. Temperature is studied only marginally, e.g. [19, 20]. Turning of the composite rods or pipes is widely used for creating recess at the end of workpieces. Composite pipes are used in the aircraft, energetic or petrochemical industry for the conduction of fluids usually such as fuel or coolants [21]. Some of these pipes are winded in multidirectional layers.

Ferreira studied turning of CFRP (Carbon Fibre Reinforced Plastics) with a fibre content of 40% and phenolic resin [22]. His work revealed the dependency of the cutting speed on cutting tool wear. He tested various cutting materials and found out that cemented carbide had flank wear of 1.5 mm after machining a length of 600 mm, while the PCD showed only 0.05 mm after a 1400-mm distance. Rahman machined by turning CFRP in his work and studied cutting tool wear for different types of material while the cutting speed was 80 m/min in maximum [23]. In accordance with previous studies, he evaluated cemented carbides as unsuitable for turning of this material.

Sreejith measured the influence of cutting conditions on the machining temperature by optical pyrometer [24]. The critical cutting speed was identified as 300 m/min in this study. The considerable increasing variability of the measured values was above this critical value. Davim studied turning of PEEK thermoplastic composite with a 30% carbon fibre content from the perspective of cutting forces [25]. A cutting tool with a positive rake angle had less steep cutting force dependence on the feed in comparison with a cutting tool with a rake angle of 0°. The tool with the positive rake angle had approximately 30% lower feed force in comparison. Mata tested the influence of cutting conditions on C/PEEK composite with various fibre

contents in a subsequent study [26]. It was found that machinability deteriorated when cutting velocity ranged from 50 to 200 m/min and feed from 0.05 to 0.2 mm. Mata dealt with cutting force prediction models using a regression analysis for machining of C/PEEK in his next study [27]. Dold used tools with laser manufactured geometry during turning of CFRP [28]. He focused on observation of differences between ground and laser machined geometry for various directions of wound composites and he measured cutting forces and surface roughness. A higher feed force was observed for a laser machined cutting tool, but surface roughness was lower in comparison with a ground cutting edge.

It is essential to understand the influence of cutting temperature on surface quality due to the very low melting point of the polymeric matrix when composite is machined. Above the melting point, it is possible to observe a steep decrease in mechanical properties, manifested by decreasing cutting force [24]. The temperature increases considerably locally in the shear zone between the cutting tool and the composite material because the polymeric matrices are poor heat conductors. This temperature can be called the cutting temperature. The cutting temperature is the average temperature of all contact points between the cutting tool and the workpiece. This temperature can be measured with a tool-work (natural) thermocouple. This thermocouple arises between the material of the cutting tool and the material of the workpiece due to their different electric potentials when the cold junction and hot junction have different temperatures. Other temperature measurement methods cannot determine cutting temperature, but rather the temperature of the point where the detector was placed or the temperature field. Davies summarized various temperature measurement methods during machining [29].

Kerrigan used an embedded (artificial) thermocouple in a cutting tool during milling operations [30]. This measurement method had a time delay in recording due to the mass of the cutting tool material between the shear zone and a K-type thermocouple placed in the cutting tool. It is disadvantageous for short-time measurement. Wang used a semi-artificial thermocouple during milling [31]. He put a thin constantan sheet between two CFRP boards. Wang observed a degradation of the resin during higher cutting speeds. The degraded resin did not support fibres well and they were easily pulled out. Masek used a similar temperature measurement principle during milling of C/PPS but using Ni-Cr wires [32]. A temperature point measurement proved that the glass transition temperature had been exceeded for all measurements in the cutting velocity ranging from 100 to 300 m/min. No degradation of the matrix was observed either on the chips or on the machined surface. Merino-Pérez introduced contactless measurement with an infrared camera on the hole exit during drilling [15]. He measured the temperature in the maxima of 250 °C and did not observe any thermal damage to the matrix. Sheik-Ahmad used an infrared camera during milling as well [33]. He compared

three different burr cutters and their influence on machining of CFRP and found that with increasing feed, more heat went to the chips due to increasing chip thickness. Yoshiro used a work-tool thermocouple during milling [34]. He observed that the glass transition temperature was exceeded for a cutting speed as low as 25 m/min. His measurement was supported with infrared camera measurement. No matrix damage was found when the machined surfaces were observed with an electron microscope.

There has been only a limited extent of experimental measurement with tool-work thermocouples during turning in machining technology, and it has been used solely for machining of metal workpieces. This method is well described for metal materials in terms of calibration as well as method measurement. The measurement itself is limited due mainly to the relatively complicated transmission of the EMF signal from the rotary to the stationary part of the thermocouple circuit. In earlier times, the signal was conducted with friction tips which had a different chemical composition than the workpiece material [35, 36]. The friction generates heat, which is conducted in the circuit of the thermocouple as the parasitic EMF signal which needs to be compensated. A more sophisticated method is to use rotation translation in a mercury bath [37–39]. The advantage of this method is parasitic signal prevention in this critical part of the thermoelectric circuit. The magnitude of the resulting EMF signal is very small and compensation or prevention of the parasitic signal is essential. The circuit must be electrically insulated from all other parts of the machine tool because induction voltage emerges in various parts of the machine tool. A problematic part is the contact of the cutting tool insert and the insert holder, which must also be insulated. This paper also addresses how to resolve this issue with cutting temperature measurement.

Electromotive force (EMF) is measured by thermocouples. EMF is the voltage which is created in the closed thermoelectric circuit between two heated materials with different electric potentials according to the Seebeck phenomena. The right temperature value must be assigned to the EMF experimentally by the calibration measurement. Calibration is valuable only for one pair of thermocouple materials. Usually the calibration is made under a flame [39], in an oven [35, 38] or in a melted metal bath [40]. The most common method is to use a special calibration setup. Calibration under a torch flame uses a metal plate as a mediator for heat conduction from the flame to the contact of a calibrated pair of metals for uniform heat conduction [41]. The temperature of the mediator plate is measured during calibration. Polymeric composites with a low matrix melting point must be heated carefully to avoid damage to the composite matrix and disconnection of the thermoelectric circuit. The design of a suitable calibration method for C/PEEK and C/PA12 materials is an important part of this paper.

The choice of cutting conditions should be conditional on reaching maximum productivity with retention of the quality parameters. Thermal damage is inadmissible during composite machining, although it has not been proven if exceeding the glass transition temperature or melting point has a significant influence on the machined surface quality after turning. This study aims on this issue as well as on the applicability of the chosen method of temperature measurement. This study focuses on the influence of the cutting conditions and cutting tool geometry on the cutting temperature when composites with a thermoplastic matrix are turned with respect to thermal effects on the machined surface. A mathematical model of the cutting temperature with significant parameters such as cutting velocity and tool geometry is presented here as well. The chosen method of the measurement was tool-work thermocouple because this only method can measure the cutting temperature. This work presents a proposal for measuring a tool-work thermocouple and a method for calibrating a tool-work thermocouple.

2 Design of experiment

2.1 Work material and cutting tool description

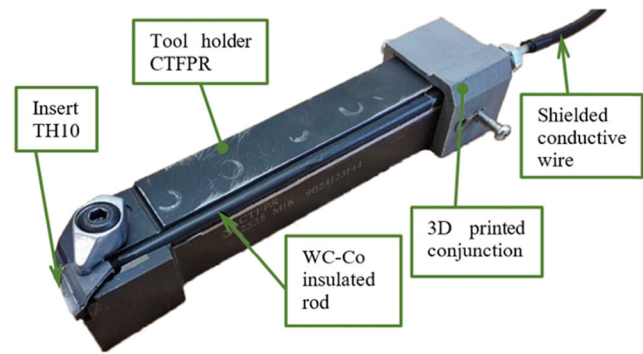
The experiment was designed for turning two types of composite materials with a thermoplastic matrix and carbon fibres, marked as C/PEEK and C/PA12. Composites were wound on a rod in tape form. Both composites had the same volume of the identical reinforcement. The properties of both materials are presented in Table 1.

The experimental setup was designed for orthogonal infeed turning of discs with a thickness of 4 mm. Both work materials were machined using a turning indexable insert TPGN type with triangle shape and with rake angle of 0° and clearance angle 11°. The inserts were processed with picosecond laser equipment to obtain various cutting edge geometries. The inserts were designed with rake angles of 0°, 10° and 20° and a clearance angle of 11° (Table 2). The cutting material was micrograin cemented carbide grade TH10 (chemical composition in volume percentages: WC (92%); NbC + TaC (2%); Co (6%)). No coating was used. The inserts were clamped in a CTFPR tool holder, which is used for an end cutting with the C type clamping of the insert using the optional chipbreaker (Fig. 1), which had a grounded bed with an inclination of 5° for the rake angle. Thus, the resulting rake angles were 5°, 15° and 25°.

The real geometry of the inserts was inspected using an Alicona InfiniteFocus G5 scanning digital microscope. The cutting edge radius and surface roughness of the chipbreakers were measured as well. The difference between the measured and designed geometry was negligible and these differences did not affect the measurements.

Table 1 Material properties of specimens

Property	Unit	Value	
Reinforcement T700 (catalogue values)			
Diameter (d_f)	μm	7	
Tensile strength (R_m)	MPa	4900	
Elongation (ϵ)	%	2.1	
Tensile strength modulus (E)	GPa	230	
Density (ρ)	g/cm^3	1.8	
Matrix (catalogue values)		PA12	PEEK
Glass transition temperature (T_g)	$^{\circ}\text{C}$	40–45	143
Melting point (T_m)	$^{\circ}\text{C}$	190	343
Tensile strength (R_m)	MPa	45	90
Elongation (ϵ)	%	300	10
Tensile strength modulus (E)	GPa	1.6	3.65
Thermal conductivity (k)	W/m K	0.23	0.25
Density (ρ)	g/cm^3	1.02	1.3
Mechanical properties of composite tapes with T700 reinforcement			
		PA12	PEEK
Short beam shear strength (SBS)	MPa	40	90
Tensile strength (G12)	MPa	1650	4650
Adhesive fracture energy (G_{Ic})	kJ/m^2	0.83	1.32
Longitudinal elastic modulus (E1)	MPa	133	142
Reinforcement volume	%	55	
Layer angle of winding on the tube	$^{\circ}$	± 65	

**Fig. 1** Modified CTFPR tool holder with 3D printed conjunction

The cutting insert holder had to be modified to decrease the parasitic EMF signal risk (Fig. 1). A carbide rod with a chemical composition similar to the indexable insert was put into the milled groove to avoid the parasitical EMF signal. The carbide rod was pushed against the insert with a screw and spring through which a wire with a small soldered ball on the end was pulled. A clamping device, which held a pushing screw, was printed by FFF from PETG polymer.

2.2 Experimental setup and cutting temperature evaluation

Turning tests were performed on a CNC lathe with a horizontal axis with a maximum spindle speed of 3150 min^{-1} , maximum power of 42 kW, maximum turning diameter of 550 mm and maximum turning length of 2500 mm. The schematic

Table 2 Carbide indexable insert parameters

Tested γ_o	0 $^{\circ}$	10 $^{\circ}$	20 $^{\circ}$
Model			
Chipbreaker schema			
Measured values of insert geometry and microgeometry			
r	3.96 μm	3.28 μm	2.1 μm
Ra	0.42 μm	0.45 μm	0.36 μm

setup is shown in Fig. 2 and real setup is in Fig. 3. The workpiece was clamped in the chuck and supported by the tailstock. Both sides of the workpiece were insulated from the machine tool by special tape, and the cutting tool was likewise insulated from the dynamometer. The compensation wire used to elongate the cutting tool branch was connected to a DAQ NI 9232 module (National Instruments). The rotary part of the workpiece branch was firstly connected to a Mercotac Type 205 slip ring, which was clamped in a special PETG 3D printed interface and mounted to the through-hole in the spindle. A software application was programmed in Labview software for the acquisition and storage of the measured data.

Before the spindle was spun, the cutting tool was set to the contact position with the workpiece. This closed the thermoelectric circuit and made it possible to read the zero value of the EMF. Then the spindle was spun, but without feed to remove a thin layer which remained from previous machining (Fig. 4). Prior to this preparation, a hump was observed at the beginning of the measured signal and for a short and quick measurement it would have affected the shape of the EMF signal significantly. The measurement under the selected cutting conditions started after the spindle had been rotating for a few seconds. The resultant EMF was calculated by subtracting the average measured EMF value from the EMF zero value.

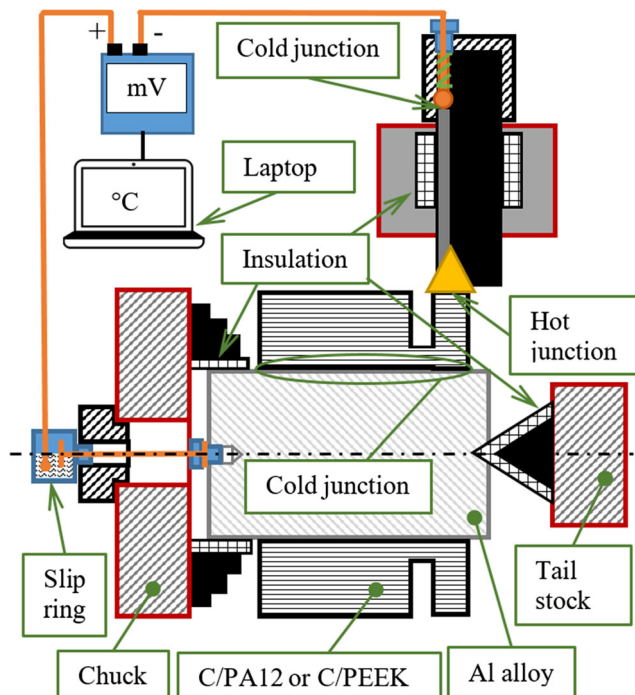


Fig. 2 Schematic design of experiment for measuring EMF to identify cutting temperature

2.3 Process of calibration

The calibration process was performed using a butadiene torch flame. The flame was adjusted to the position in front of the conjunction of the tool and workpiece and thermocouple K. EMF and temperature were detected simultaneously by an ALMEMO measuring station from AHLBORN. When the calibration temperature reached approximately 800 °C, the measurement was interrupted, the flame was turned off and cooling took place spontaneously. Almost the same circuit that was used for calibration was used for the experimental measurements. It was not possible to use this design because the carbide rod disconnected from the insert due to the extensive heat from the torch. Thus, the insert was removed from the cutting tool branch of the circuit. A workpiece and cutting tool branch were connected to the ALMEMO as well as the thermocouple (type K) for the temperature measurement (Fig. 5). The calibration was repeated five times for statistical evaluation of the measured data and uncertainty evaluation.

2.4 Evaluation of the chips

Chips were collected during machining and compared to one another for heat damage investigation. Subsequently, several typical chips for each test were photographed using an optical microscope by LIM (Laboratory Imaging s.r.o.) with up to 50 times optical zoom (Fig. 6). Photographs of the tool side and workpiece side of the chips were taken with the microscope. Macro photographs of the chips were taken with a Canon EOS 550D digital camera.

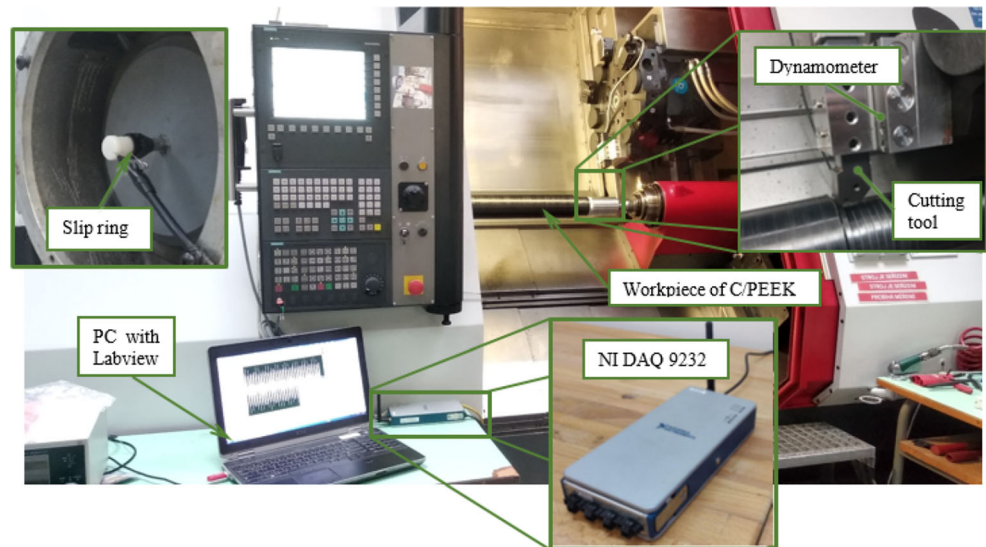
2.5 Evaluation of machined surface

The machined surface could be affected by heat. The machined surface was evaluated by optical method and by surface roughness measurement. Photographs were taken with a digital optical microscope from LIM. Surface roughness was measured with a Surtronic 3+ portable, self-contained instrument (Fig. 7). Surface roughness was measured perpendicular to the cutting velocity vector. Ra parameter of surface roughness was evaluated five times in each run of the experiment. The surface deformation demonstrates the influence of the cutting conditions of heat and force.

2.6 Investigation of the structural changes to the workpiece

A structural change can be observed in the polymers when they are affected by heat. Structural changes are manifested by a change in the melting point value. DSC (differential scanning calorimetry) was chosen for evaluation of the melting point for the composites C/PA12 and C/PEEK after affecting by heat in regards to machining. A NETZSCH STA 409

Fig. 3 Setup of experiment on the turning centre



PG LUXX thermal analysis device was used. A heating rate of 10 °C/min was selected per the EN ISO 11357-1 standard. The real cooling rate was 3 to 2 °C.

The differential scanning calorimetry (DSC) method is suitable for revealing the thermal history of the tested polymer. In this case, we examined whether any change to the crystalline structure had occurred under high temperature. This would be manifested by a change in the crystallization temperature of the polymer. It was necessary to obtain one specimen whose temperature was not affected by machining, one unmachined specimen and one with a high measured temperature. In the reference [42], Pomeranke described the possibility of using this method for the analysis of crystallization temperature changes in polymers after heating.

2.7 Measurement

The experiment design had five cutting velocity levels ranging from 100 to 300 m/min and two feed values of 0.15 mm and 0.3 mm. Cutting tools with three different rake angles, namely

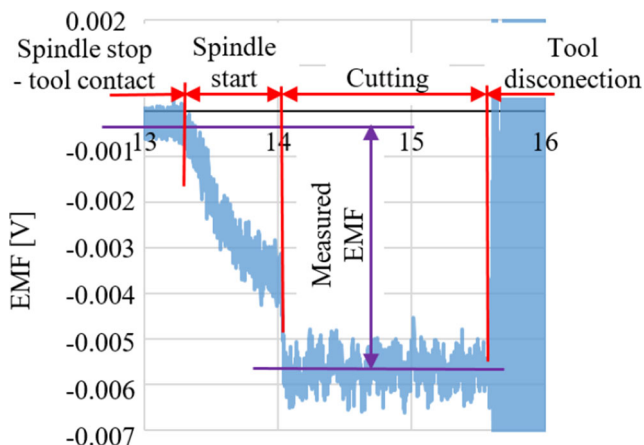


Fig. 4 Evaluation of the EMF signal principle

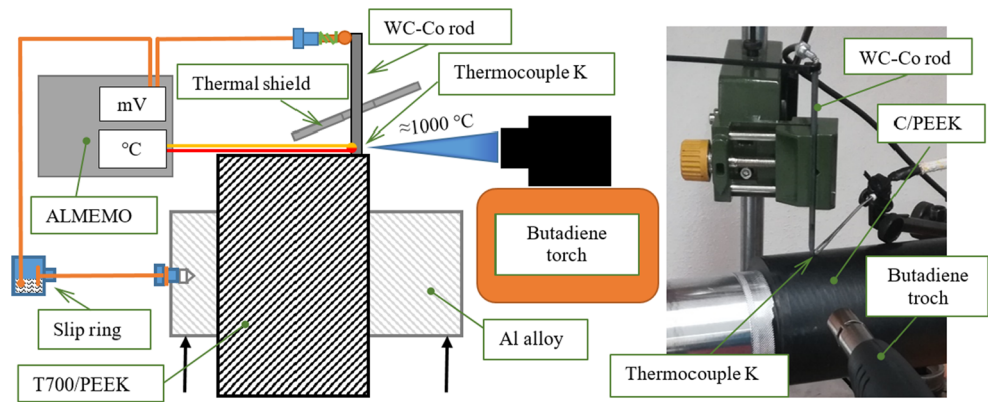
5°, 15° and 25°, were tested. The experiment was performed in three repetitions. Moreover, the number of repetitions was increased to 6 for specific combinations of parameters ($v_c = 100$ m/min; $f = 0.15$ mm; $\gamma_o = 5^\circ$) to express measurement uncertainty. The values of these parameters are highlighted in Table 3. These values were chosen in order to obtain a better quality of the EMF record, which was slightly easier to read for smaller cutting conditions than for higher ones due to the dynamic effects of the cutting process.

3 Results and discussion

3.1 Calibration of the thermocouple and uncertainty of measurement assessment

Taking measurements with a tool-work thermocouple enables documentation of the cutting temperature — i.e. the mean of the temperatures in all contact joints between the cutting tool and workpiece during machining. It is the temperature not only on the cutting edge but also on the small part of the rake and clearance face depending on the cutting edge engage conditions. Cutting temperature is the highest temperature which can be measured during machining. The main disadvantage of this measurement method is that it requires calibration, which is complicated for polymeric composites due to the low matrix melting point and it was a significant source of uncertainty. Butadiene torch calibration was chosen mainly because it allowed use of an unchanged workpiece and cutting tool without requiring manufacture of another calibration setup. The main setup used during the experimental machining was changed only slightly and the indexable insert was removed. This setup gave a stable EMF signal under intensive torch heating and the thermoelectric circuit was stable. The difference between the indexable insert and the carbide rod was

Fig. 5 Calibration of T700 – WC-Co rod thermocouple: schematic (left), photo of actual setup (right)



neglected due to the similarity of the chemical composition of the two types of carbide and became the uncertainty of the measurement. The temperature on the measured part was gradually increased up to 800 °C on the C/PEEK composite. The tested specimen was locally deformed by this intense heat.

The same calibration curve was valid for C/PA12 and C/PEEK also because both have the same type of carbon fibres and volume. The measured data were interspersed by polynomial function regression analysis and then prediction intervals were defined for evaluation of uncertainty. The calculated equation of the calibration curve had a determination coefficient of 0.997 (Fig. 8). That is proof that the established model fits measured data well. The calibration curve equation that was obtained for the calculation of the cutting temperature (Θ) is presented below by Eq. (1).

$$\Theta = -0.0234 \cdot EMF^5 + 0.6089 \cdot EMF^4 - 6.1079 \cdot EMF^3 + 26.332 \cdot EMF^2 + 48.768 \cdot EMF + 26.714 \quad (1)$$

The measurement uncertainty is the range of values which may be assigned to the measured values and it should be

defined for each new measurement setup. The uncertainty of the calibration curve was given by the width of the prediction interval (PI) in which the value of the measured cutting temperature is correct and may be identified with the given EMF value with 95 % probability. The width of the prediction interval was on average ± 14.52 °C. Uncertainty from other sources was added to this prediction interval. The only uncertainty source was the ALMEMO 5690-2CPU in this case, specifically the uncertainty coupled with the voltage measurement error and uncertainty coupled with the error of the temperature measurement measured with a K-type thermocouple. The resulting calibration uncertainty was $u_b = 14.59$ °C and this was not a relevant difference from the prediction interval alone.

Uncertainty type A is the uncertainty calculated directly from a number of measurements and is equal to the corrected sampling standard deviation. The determination of this type of uncertainty was performed from an experiment with an increased number of replications under cutting conditions ($v_c = 100$ m/min; $f = 0.15$ mm; $\gamma_o = 5^\circ$). The average temperature measured for C/PA12 was 324 °C with uncertainty $u_a = 8.11$ °C. The resulting uncertainty with calculated calibration measurement uncertainty was $u_c = 16.69$ °C for material C/PA12 for the given cutting conditions. The resulting description of uncertainty was (323.88 ± 16.69) °C for material C/PA12.

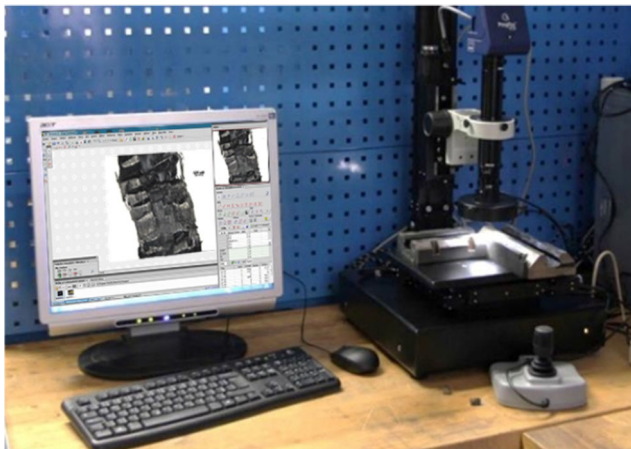


Fig. 6 LIM microscope — chips and surface measurement



Fig. 7 Surtronic 3+ - Surface roughness measurement

Table 3 Design of full factorial experiment — cutting parameters

Parameter/factor			Level				
			1	2	3	4	5
Cutting velocity	m/min	v_c	100	150	200	250	300
Feed per revolution	mm	f	0.15	0.3			
Rake angle	°	γ_o	5	15	25		

The average temperature measured for C/PEEK was 530°C with uncertainty $u_d = 7.25$ °C. The resulting uncertainty was $u_c = 16.29$ °C and the resulting description of uncertainty was (530.28 ± 16.29) °C for the C/PEEK material.

3.2 Evaluation of the cutting temperature measurement

Cutting temperature was measured almost always above the melting point of tested matrices. The cutting temperature was nearest to the melting point when C/PA12 was measured (Figs. 12, 13, 14 and 15). Relative increment of cutting temperature above melting point was only a little bit different for both tested materials. This high temperature should affect both the machined surface and the chips. For this reason, the machined surface and chips were measured and evaluated. The results of these measurements are described in the following text.

The measured values were analysed using the ANOVA method. Statistically significant parameters were revealed and then used to determine the predictive mathematical model for calculation of the cutting temperature. It is possible to reject the null hypothesis about equal variances at a

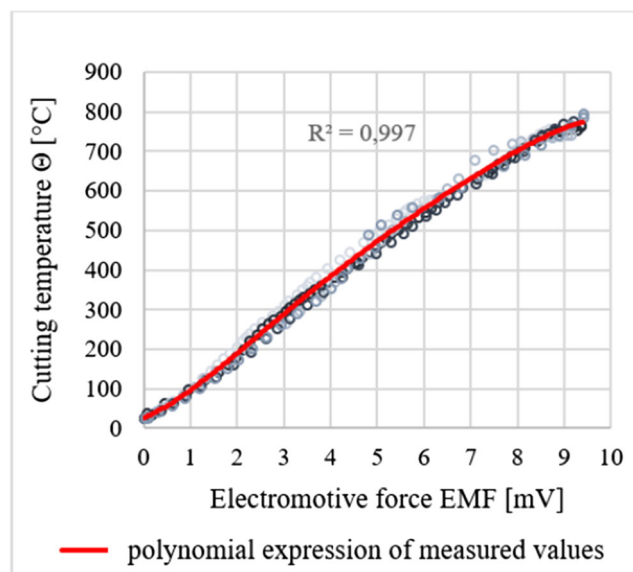
significance level of $\alpha = 0.05$ from the results of p-values for control factors v_c and γ_o for both tested materials (Table 4 and Table 5). That means that the only statistically insignificant factor was feed. Control factors v_c and γ_o are almost equal in statistical significance on the basis of the value F.

In C/PA12 machining, the most important factor was the cutting speed, but the difference in F value for the cutting speed and the rake angle was relatively small. The opposite result was found for C/PEEK, where the cutting speed had a smaller value of F than the rake angle. However, the difference between them was again small. A higher rake angle leads to less deformation in the primary cutting zone and a lower cutting temperature. The cutting speed has the most significant effect on the cutting temperature and the results of this study were consistent with this well-known fact.

The main effect plot for the cutting temperature mean describes the behaviour of temperature with the changing control factor (Fig. 9). It is possible to compare the two tested materials at once. C/PA12 generated a cutting temperature about 201 °C lower on average. The cutting temperature grew with cutting velocity nonlinearly for both the tested composite materials. This dependence was similar to the power function which was used to design the predictive model. Contrarily, the increasing rake angle decreased the cutting temperature linearly. The feed had no influence and remains almost horizontal in the diagram.

The measured cutting temperature was almost always above the melting point of the tested matrices. The cutting temperature was closest to the melting point when C/PA12 was measured, but the ratio of the cutting temperature and melting point was almost identical for the two materials. The relative increment of the cutting temperature above the melting point was only slightly different for each of the tested materials.

A recommendation might be to decrease the cutting velocity at first when the thermal defects occur. The rake angle was also statistically significant. The cutting temperature

**Fig. 8** Calibration curve T700 – WC-Co for cutting temperature**Table 4** Results of ANOVA test for C/PA12 composite

Source	DF	Seq SS	Adj SS	Adj MS	P (%)	F	p-value
v_c	4	73309	72143	18036	65.1	88.65	0
f	1	177	43	43	0.2	0.21	0.648
γ_o	2	33084	33084	16542	29.3	81.3	0
Error	30	6104	6104	203	5.4		
Total	37	112673					

DF degrees of freedom, Seq SS sequential sum of squares, Adj SS adjusted sum of squares, Adj MS adjusted mean squares – variance around fitted value, P (%)percentage of contribution, F F-value (test static), p-value (probability)

Table 5 Results of ANOVA test for C/PEEK composite

Source	DF	Seq SS	Adj SS	Adj MS	P (%)	F	p-value
v_c	4	50393	50393	12598	61.7	135.39	0
f	1	132	132	132	0.2	1.42	0.242
γ_o	2	27920	27920	13960	34.2	150.03	0
Error	34	3164	3164	93	3.9		
Total	41	81609					

decreased with increasing rake angle. A greater rake angle effect was measured for C/PA12. The PA12 matrix was the softer of the two tested matrices and it was able to undergo bigger plastic deformation during chip formation. The area of primary plastic deformation decreased and inclined towards the rake face of the cutting tool and the change of primary plastic deformation was greater than for the PEEK matrix due to the ability of PA12 to deform most easily. A linearity of cutting velocity dependency on rake angle was observed for both tested materials. The feed per revolution was evaluated as statistically insignificant. Increasing the feed is one major way to increase productivity without the risk of thermal defects but only until delamination issues occur.

3.3 Cutting temperature models

As expected, the cutting temperature was most sensitive to cutting velocity. The power function was estimated for this dependence. This mathematical representation corresponded with practical measurement of other metallic materials. This corresponds with practical measurements and with metallic material machining theory as well. The increment of the cutting temperature with cutting velocity was smaller for C/PEEK than for C/PA12 due to the lower deformation ability of the PEEK matrix. The second very important parameter of the cutting temperature model was the rake angle. Feed, as the insignificant control factor, was not included in the model.

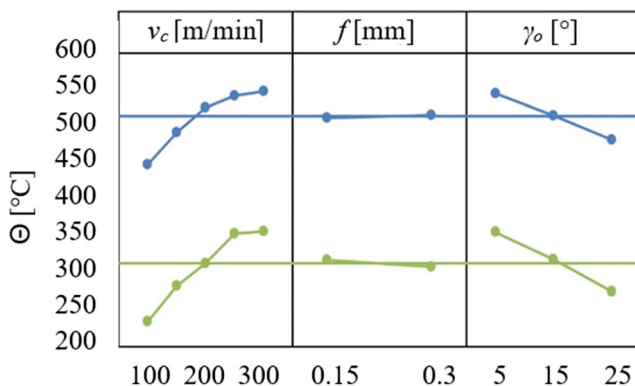


Fig. 9 Main effect plot for cutting temperature mean for C/PA12 (green) and C/PEEK (blue)

The model was determined for the most suitable mathematical interpretation with the best statistical fit. The equation was the same for both tested materials.

$$= A^* v_c^B + \gamma^* C \quad (2)$$

The coefficients for C/PA12 and C/PEEK were estimated by iterations in Minitab 16 software. The proposed parameters of the model equation are shown in Table 6 and Table 7.

The estimated coefficient C (for the rake angle) was very similar for both tested materials. The same coefficient was chosen for both materials ($C = -3.5$) due to the generalization of the model. The rest of the model coefficients were recalculated for these new entry conditions. The results of the newly estimated coefficients are shown in Table 8 and Table 9.

The model equation with the proposed coefficients for material C/PA12 was tested by the Lack-of-fit method (Table 10). As follows from evaluation of this test, there was no evidence demonstrating that this model did not fit the experimental data at a significance level of $\alpha = 0.05$.

The model equation with the proposed coefficients for material C/PEEK was also tested by the Lack-of-fit method (Table 11). As follows from evaluation of this test, in this case as well there was not any evidence that this model did not fit the experimental data at a significance level of $\alpha = 0.05$.

The measured data were compared with the model graphically. The predictive model respected the measured data and went through almost all measured points (Fig. 10 and Fig. 11) for material C/PA12 and also for C/PEEK (Fig. 12 and Fig. 13).

3.4 Evaluation of chips and machined surface

Neither the chips nor the machined surface showed any obvious thermal damage. Thermoplastic materials should become softer above the glass transition temperature due to elongation of polymeric chains. The high temperature in the shear zone could be a cause of the ribbon chips observed whenever the C/PA12 material was machined and C/PEEK on the small feeds and small rake angle. It was possible to get small segmented chips for C/PEEK (Table 12) when the feed was increased and the high rake angle was used. In this case, the

Table 6 Estimation of parameter for model — C/PA12

Parameter	Estimate	SE	Estimate 95% CI	
A	71.1927	8.71	(55.22;	91.02)
B	0.3152	0.22	(0.27;	0.36)
C	-3.9813	0.36	(-4.72;	-3.24)

SE standard error, CI confidential interval

Table 7 Estimation of parameter for model — C/PEEK

Parameter	Estimate	SE	Estimate 95% CI	
A	228.99	13.17	(203.47;	257.32)
B	0.17	0.011	(0.15;	0.19)
C	− 3.32	0.272	(− 3.79;	− 2.68)

chips sometimes curled themselves into flat spirals. If the radius of spiralling exceeded a particular diameter, the chips leaned on the unmachined surface and broke off. This phenomena was probably not affected by temperature because it seems to be independent of the cutting velocity. The chips are smoother on the tool side. The cracking of fibres was observable on the workpiece side of the chips. This was accompanied by observed waves of the matrix on the workpiece side of the chips which bond cracked chips. These waves occurred mainly under high cutting velocities.

The chips of the C/PA12 were all ribbon and snarled under various cutting conditions (Table 13). C/PA12 was machined closer to the melting point than C/PEEK. We observed smooth tool sides on the chips for all measurements. A cracking of the reinforcements was observed on the workpiece side of the chips. The chips broke into smaller ribbons when high feed and cutting speed was applied and a high rake angle was used. The combination of chip. The high rake angle together with the optional chipbreaker created shorter chips. The chips were curled in a smaller radius than when a smaller rake angle was used. If the chipbreaker was not used, the chip deformation would be smaller for a larger rake angle. Chip deformation for G/PEEK was evaluated by Davim and his results showed less chip deformation with higher rake angle [43]. No heat damage sign was found in the C/PA12 after optical measurement by the LIM microscope.

The machined surface was photographed with a microscope (Table 14). No negative effect of heat on the machined surface was observed, although the cutting temperature was higher in each run of the experiment than the melting point of the matrix. The machined surface was more affected in the case of C/PA12 after turning than for C/PEEK. The machined surfaces seemed to be slightly worse when the rake angle of

Table 9 Second estimation of model parameters — C/PEEK

Parameter	Estimate	SE	Estimate 95% CI	
A	232.125	12.86	207.29	259.76
B	0.169	0.011	0.15	0.19
C	− 3.5			

the cutting tool was small. The cutting conditions did not have any visible influence on the machined surface.

Photographs of the machined surfaces were supplemented by surface roughness measurements. Surface roughness was evaluated by Ra parameter and measurements were made perpendicular to the main cutting movement, which was the only usable direction for measurement in the machine tool. The measured surface roughness of C/PA12 was twice that of C/PEEK. The cutting temperature most likely melted spikes of roughness and made the surface smoother. The effect of surface roughness was also proven for C/PEEK but only to a limited extent. Variations of the measured data were higher than the differences between rake angle levels. A significant influence of the rake angle on the surface roughness was measured mainly for C/PA12 where the differences between the measurements were higher than for C/PEEK. The surface roughness increased with rake angle (Fig. 14 and Fig. 15). Only very small differences in surface roughness were observed when the cutting velocity was changed. It seemed that the difference between the minimum and maximum rake angle decreased when the cutting velocity was increased. However, it can be stated that the increase in cutting speed led to less surface roughness. This corresponds to the study published by Davim and Reis [44].

3.5 Results of DSC structural changes measurement

Three specimens were required to obtain DSC analysis: one unmachined specimen, the other machined but not affected by heat, and the third machined with heat. The first specimen was taken from the unmachined surface layer of the workpiece. The second and third specimens were chips taken under specific cutting conditions. Each of the specimen was burned in a calorimeter's heat chamber and the thermal energy required to raise the temperature was measured.

Table 8 Second estimation of model parameters — C/P12

Parameter	Estimate	SE	Estimate 95% CI	
A	67.52	8.1	52.78	86.05
B	0.32	0.02	0.28	0.37
C	− 3.5			

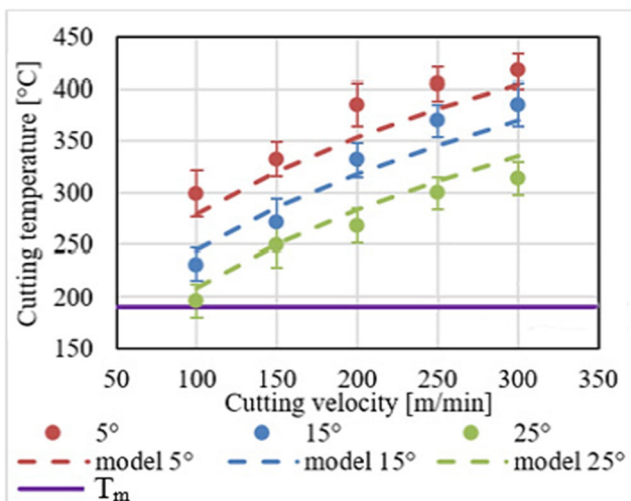
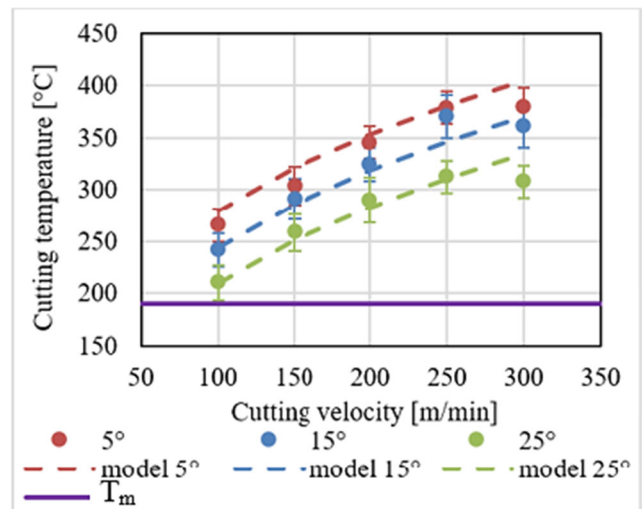
Table 10 Lack-of-fit evaluation for C/PA12

Source	DF	SS	MS	F	P
Error	28	7547	269.541		
Lack of fit	13	3376.52	259.733	0.93	0.545
Pure error	15	4170.64	278.042		

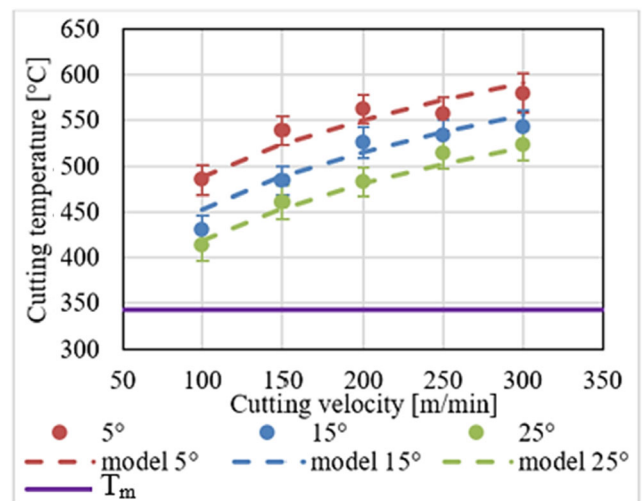
Table 11 Lack-of-fit evaluation for C/PEEK

Source	DF	SS	MS	F	P
Error	28	4125.06	147.324		
Lack of fit	13	2746.84	211.295	2.3	0.063
Pure error	15	1378.22	91.882		

After interpolation of the cutting temperature model, it was predicted that the unaffected machined specimen should be machined with a cutting velocity of approx. 10 m/min for both tested polymeric matrices. This estimation could be inaccurate because this small value of the cutting velocity was very far from the selected and verified range of cutting velocities of the cutting temperature model. Up to this value of the cutting velocity, it should not matter what values of the rake angle and the feed rate are selected. The measured temperature should be below the melting point during turning. An experiment proved that the measured cutting temperatures were below the melting point for cutting conditions: $v_c = 10$ m/min, $f = 0.15$ mm and $\gamma_o = 5^\circ$. The measured cutting temperature was 85 °C for C/PEEK and 55° for C/PA12. The cutting temperature model overestimated by almost three times the value of cutting temperatures for both tested composites using the above mentioned cutting conditions. The other machined specimen was machined under a cutting velocity of 300 m/min. The temperature measured under this cutting velocity was far above the melting point for both specimens. The feed rate and rake angle remain the same as the previous specimen. In principle, three samples were measured by the DSC method to determinate the crystalline temperature during cooling from the high temperature. Crystallization temperatures of the machined specimens were compared to one another.

**Fig. 10** Comparison of measured data and model function for C/PA12 ($f = 0.15$ mm)**Fig. 11** Comparison of measured data and model function for C/PA12 ($f = 0.3$ mm)

The first C/PA12 unmachined specimen was heated to a temperature of 350 °C (green line, Fig. 16). When it had cooled, crystallization was observed at a temperature of 152 °C. The crystallization temperature shifted to a lower temperature due to the change in the polymeric structure. The second specimen (red line, Fig. 16), machined at $v_c = 300$ m/min, was heated to the melting point and then cooled. The crystallization temperature was 158 °C. The third specimen (blue line, Fig. 16) machined at $v_c = 10$ m/min was tested in the same way as the second one. The crystallization temperature was the same as for the second specimen. This result means that there is no evidence of thermal effects on the specimen machined at the $v_c = 300$ m/min causing a change of the crystalline structure of the polymer in the entire volume of the test specimen. It is possible that the cutting temperature did not affect the bigger volume of the material from the cutting zone and the DSC method was unable to reveal the

**Fig. 12** Comparison of measured data and model function for C/PEEK ($f = 0.15$ mm)

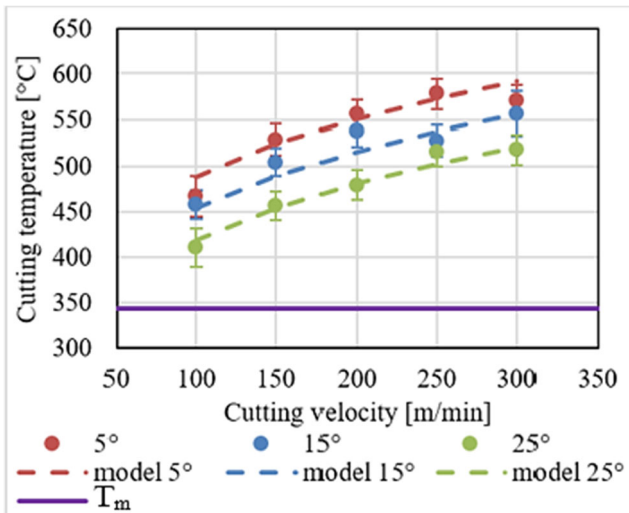


Fig. 13 Comparison of measured data and model function for C/PEEK ($f = 0.3$ mm)

change of crystallization temperature. The second possibility is the inaccuracy of the tool-work for two-component composites. Only carbon fibres are the conductor of the EMF

signal. However, carbon fibres have significantly higher mechanical properties than matrices. In our opinion, fibres deformation requires higher energy and very likely generates more heat during machining than the polymer matrix that binds fibres. However, the fibre volume was 55 % and the thermal conductivity of the polymer could inhibited equally conduction of the heat to the entire volume of the chip or machined surface. The resulting heat would then be less than the heat indicated by the measured temperatures. It was assumed that the total weight of the machined specimens was affected by heat. However, poor thermal conductivity of the polymers could cause the temperature of the contact points between the cutting tool edge and the front side of the chip to be higher than the back side of the chip. These unverified speculations could be the reason why the change in the crystalline structure was not detected in polymers by DSC. An additional experimental investigation could be made for verifying this hypothesis in the future.

The C/PEEK material was tested by the DSC method in the same way (Fig. 17). The first unmachined specimen (green line, Fig. 17) was heated up to a temperature of 530 °C. That

Table 12 Comparison of C/PEEK chips under various cutting conditions

C /PEEK	$v_c = 150$ m/min $f = 0.15$ mm $\gamma_o = 5^\circ$	$v_c = 150$ m/min $f = 0.3$ mm $\gamma_o = 5^\circ$	$v_c = 300$ m/min $f = 0.15$ mm $\gamma_o = 25^\circ$	$v_c = 300$ m/min $f = 0.3$ mm $\gamma_o = 25^\circ$
Front side of the chip				
Back side of the chip				
Shape of the chip				

Table 13 Comparison of C/PA12 chips under various cutting conditions


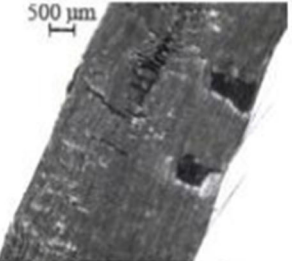
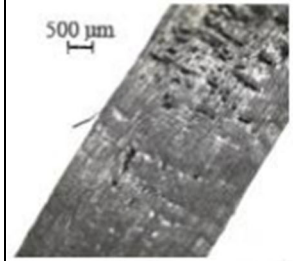
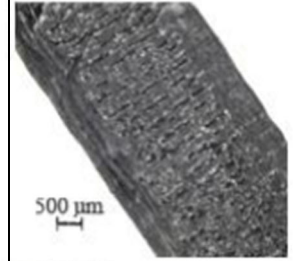

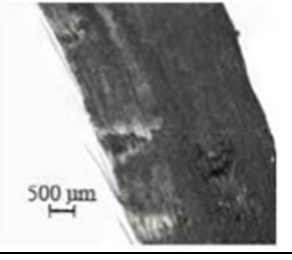
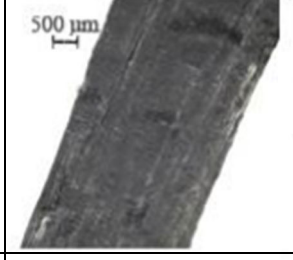
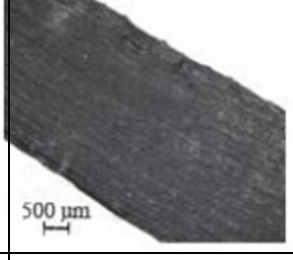
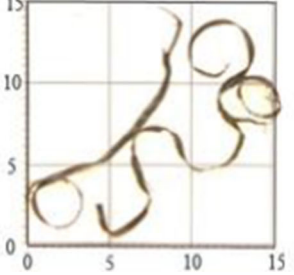
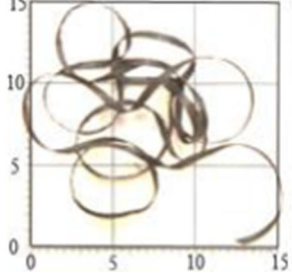
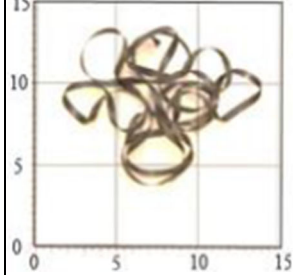
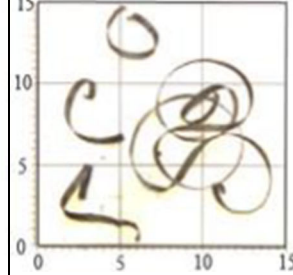

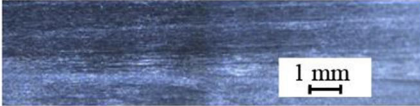
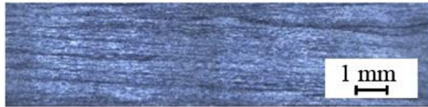
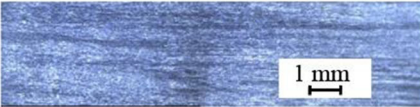
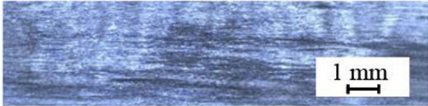
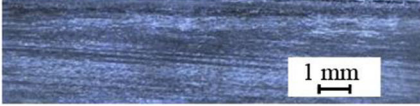
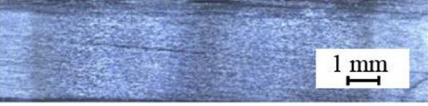
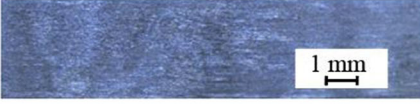
C/PA12	$v_c = 150$ m/min $f = 0.15$ mm $\gamma_o = 5^\circ$	$v_c = 150$ m/min $f = 0.3$ mm $\gamma_o = 5^\circ$	$v_c = 300$ m/min $f = 0.15$ mm $\gamma_o = 25^\circ$	$v_c = 300$ m/min $f = 0.3$ mm $\gamma_o = 25^\circ$
Front side of the chip				
Back side of the chip				
Shape of the chip				

Table 14 Comparison of machined surface for C/PEEK and C/PA12 under different cutting conditions

	$v_c = 150$ m/min $f = 0.15$ mm	$v_c = 300$ m/min $f = 0.15$ mm
C/PEEK	$\gamma_o = 5^\circ$ 	$\gamma_o = 5^\circ$ 
	$\gamma_o = 25^\circ$ 	$\gamma_o = 25^\circ$ 
C/PA12	$\gamma_o = 5^\circ$ 	$\gamma_o = 5^\circ$ 
	$\gamma_o = 25^\circ$ 	$\gamma_o = 25^\circ$ 

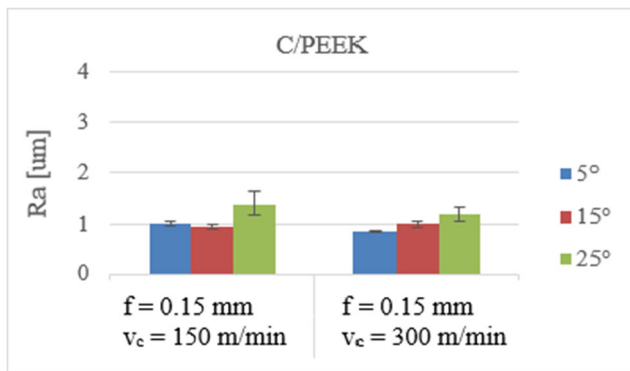


Fig. 14 Surface roughness comparison under various cutting conditions C/PEEK

was the highest measured temperature by the tool-work thermocouple. The crystallization temperature was not observed at all during cooling. The measurement was ended when a temperature of 200 °C was reached. The crystallization temperature should probably be lower. The crystallization temperature for both machined specimens was the same – 280 °C.

The DSC method did not reveal any evidences that chips were affected by the heat, which is consistent with [34] and [15] where SEM was used to the inspection of the heat effect on the composites. It is possible that the measured temperature affected only a small volume cut material, or the temperature measured by T700 – WC-Co thermocouple did not represent a real temperature in the cutting zone due to differences in the thermal properties of the reinforcement and the matrix. DSC method proved that the chosen composites were not heat affected by turning, although the glass transition temperature and also melting point were exceed.

4 Conclusion

In this paper, we proposed and verified a cutting temperature measurement method for carbon fibre reinforced plastic during turning by a tool-work thermocouple. Electrically conductive carbon fibres were used as a part of a thermoelectric

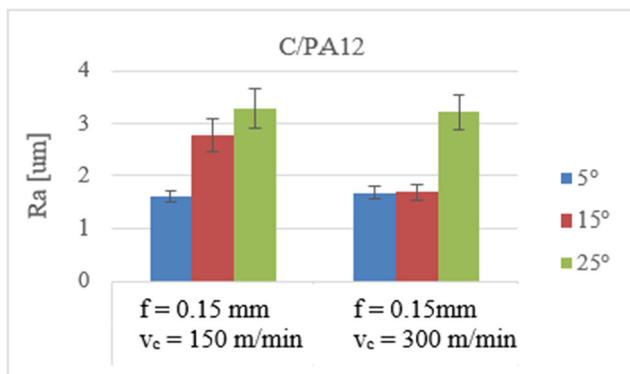


Fig. 15 Surface roughness comparison under various cutting conditions C/PA12

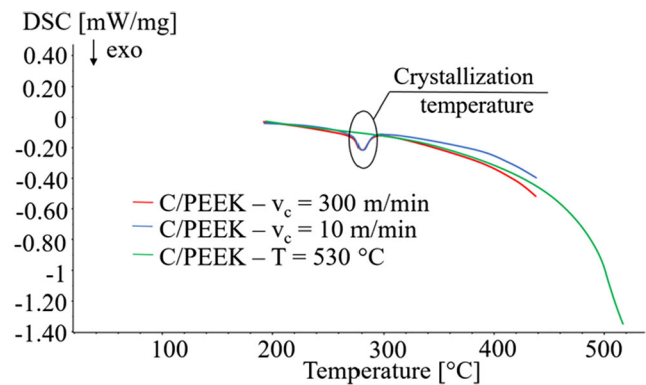


Fig. 16 Cooling curves for C/PEEK – DSC method

circuit. The calibration of the tool-work thermocouple was performed under a butadiene torch flame. This relatively well-known measurement method was used for the first time for this application. The main task was to determine the effect of cutting temperature on thermal damage of machined composites. The calibration of T700 – WC-Co was valid with the uncertainty of the measurement ± 15 °C. Work with the tool-work thermocouple was verified on a group of measurements for two CFRP materials, C/PA12 and C/PEEK. This measurement setting was relatively reliable and will be used in the future to further measurement of the cutting temperature of various metals and alloys with some improvements. The verification measurements led to these conclusions:

- The cutting temperature was dependent on the cutting velocity in the form of a power function in accordance with the theory of metal materials for both CFRPs.
- A positive influence on decreasing cutting temperature was observed with increasing rake angle.
- The measured effect of feed per revolution on cutting temperature was zero or very small.

Cutting temperature models for two composite materials have been proposed. The coefficients of the model equation were calculated from all measured data. These temperature

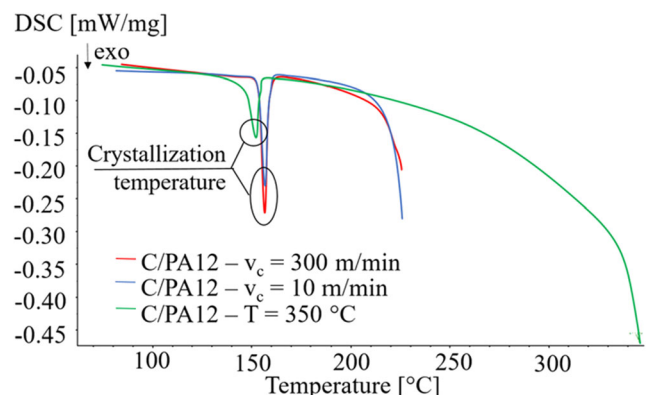


Fig. 17 Cooling curves for C/PA12 – DSC method

models correspond to the measured data according to the statistical evaluation in the given range of the cutting conditions and the cutting tool geometry ($v_c = 100$ to 300 m/min and $\gamma_o = 5^\circ$ to 25°). The cutting temperature model was designed and the equation coefficients were calculated from all of the measured data. This model was generalized for rake angle influence. Other coefficients were taken as material constants. The resultant model had verified conformity with the measured data according to the lack-of-fit test for both tested materials. These models can be used for practical application or for subsequent research. Future work will focus on the effect of cutting conditions on cutting forces for C/PA12 and C/PEEK composites.

There is no or only weak evidence of thermal deflection for the machined surface and for the chips, although all measured values were above the melting point according to the tool-work thermocouple method of cutting temperature measurement. The DSC method was used to examine the change in crystallization temperature after previous heat treatment, and this method did not reveal the difference between heat-affected and non-heat-affected specimens.

Additional measurements of surface roughness proved the negative influence of increasing rake angle. C/PA12 had a higher surface roughness than C/PEEK. The rake angle had a significant effect on both composites, but more significant on C/PA12 than on C/PEEK.

Author contribution Not applicable.

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Data availability Not applicable.

Code availability Not applicable.

Declarations

Competing interests The authors declare no competing interests.

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